

Interactive comment on “ArduiTaM: accurate and inexpensive NMR auto tune and match system” by Mazin Jouda et al.
Mazin Jouda et al.

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Reviewer 1:

Authors: First of all, we would like to thank the reviewer for giving the time and effort to reviewing our manuscript.

Reviewer: General remarks: This contribution offers a way of automated tuning and matching in NMR and MRI using an open-source hardware and software solution with a single board microcontroller. This maybe a good approach for from scratch new system design and refurbishing of older systems. With current commercial NMR probes we are not sure such a system can help to work around some of the commonly encountered problem, that is mechanical hysteresis and slip of the controller rods connecting the stepper motors to the capacitors. A software that “learns” this non ideal behavior of probes (which is also subject to aging) and can manipulate the actuators more efficiently than a human would be nice. In a production environment (i.e. with high throughput).

Authors: This is a very interesting idea, although the ideal solution would be to make the mechanical system (trimmers, rods, etc.) robust against aging and hysteresis, if not permanently then at least for some long enough time after which the mechanical system can be renewed. Nevertheless, the idea of involving "learning" algorithms is very motivating and can definitely provide solutions to circumvent the mechanical hysteresis problem, and can probably make T&M faster. Just like the difference between a new NMR user and an experienced user.

Reviewer: The method for tuning and matching is not fundamentally “new” as it relies on the well known rf-responses exploited by current commercial hardware. The speed of the process is apparently better, but it is not clear, if the same goal couldn’t be achieved by an adaptive software implementation with existing hardware. Where the proposed solution may be highly beneficial are probes going beyond the current mechanical trimmer capacitor based system using varactors or digital capacitors, as the authors emphasize. NB: I have been looking at the paper mostly from a spectroscopy perspective. Some of my arguments may not apply in an imaging context.

Reviewer: Specific questions and comments: In the “homing routine” for driving the capacitors to their lowest values: How is the stop detected? Steppers do not usually sense that they are stuck and absolute positioning may not maintained when restarting the Arduino. Is there absolute angle sensing on the steppers? Is there a provision against excessive torque being applied?

Authors: The current implementation requires the user to do one-time single-point calibration of the tuning and matching capacitors when attaching ArduiTaM for the first time. This can be easily done by manually rotating the trimmers to their lower value which is recognized by

ArduiTaM as the zero position, and by setting the allowed number of turns before the upper value is reached. As long as it is not turned off, ArduiTaM can keep track of stepper motors' positions and ensure that neither limit is exceeded. A simple modification of the code, such that current positions the trimmers are written in the EEPROM of the Arduino, would allow ArduiTaM to keep track of the stepper motors' positions even after being completely powered off. If this one-time single-point calibration step is to be avoided, then a couple of limit switches for the tuning and matching trimmers would be required.

We have added a paragraph (lines: 136-142) to clarify this point

Reviewer: About the steppers: 20 steps per turn sounds like a low number. Could a gearbox be added achieve lower angles. But that could increase the mechanical instability. The first scan of the two capacitors appears to be quite coarse. Depending on the type of probe (high resolution liquids vs. static solids, for example you may miss the actual minimum (multiply tuned probes may have several minima).

Authors: We are extremely sorry for this typo. In fact the stepper motors we used are SM-42BYG011-25 and have a 1.8 degree/step resolution, thus requiring 200 steps per turn. With this high resolution, it is very unlikely to miss the actual minimum, and that is probably why we never encountered this problem during the experiments. Nevertheless, this is a very valid point and suggests that one has to be very careful when selecting a stepper motor or defining the sweep resolution. Indeed, having a higher stepping resolution and a finer sweep would likely guarantee finding the minimum, but that is unfortunately at the expense of prolonged T&M time.

We have corrected these values in the manuscript (lines: 127, 128)

Reviewer: How does the algorithm handle the sudden “jumps” when changing the capacitances (as experienced in manual tuning T&M, likely caused by release of torsional stress in long connection rods? This is a big problem, also for commercial systems and is (in my opinion) the reason for suboptimal T&M in existing systems.

Authors: In fact, we did not encounter this problem during the experiments. This is probably because the mechanical setup was newly built and we used new high quality trimmers and stiff glass fiber rods. Another potential reason is the relatively low operating frequency (45 MHz) where slight capacitance changes are less pronounced. From our experience, we know that trimmer capacitors become loose after going through many tuning cycles. This is most likely the reason behind these jumps. In such a case, the ideal remedy would be to replace the trimmers with fresh ones. Alternatively, one can think of a software solution by always comparing three or four consecutive S11 points and check for dramatic jumps so that incorrect points can be reacquired.

Reviewer: Could the hardware/software combo be extended to other tuning/matching modalities, like frequency pushing effects or spin noise? [J Mag Res 193 (2008) 153; J Biomol NMR 45 (2009) 241; ChemPhysChem 15 (2014) 3639] Considering the fact that the impedance of the pre-amplifier and the transmission line from the rf-coil to the pre-amp play a major role in high efficiency tuning, the scope of the approach, which apparently requires switching between the

envelope detector and the proper detection preamplifier may be applicable to, for example, cryogenically cooled probes.

Authors: The short answer is yes! The long answer is as follows; ideally, both the output impedance of the power amplifier and the input impedance of the preamplifier should be exactly equal to the characteristic impedance of the coaxial cables (usually 50 Ohm). If this is the case, then matching the coil in the excitation phase by minimizing its reflected power necessarily means that the coil will also be matched to the preamplifier in the reception phase. Practically, these impedances as well as the characteristic impedance of the coaxial cable might slightly differ from 50 Ohm resulting in slight discrepancy between the matching conditions in the excitation and reception phases. Usually this discrepancy is small and thus negligible. However, it might become significant in certain circumstances as for example high frequency systems and high Q probes. In such cases, one solution to tackle this problem is to measure this discrepancy on the spectrometer where ArduiTaM is to be installed and to feed this measurement as an offset frequency to the ArduiTaM such that when the minimum reflection is achieved in the excitation phase at the offset frequency the matching condition is fulfilled in the reception phase at the Larmor frequency. This should work robustly as long as the Larmor frequency does not drift considerably.

Conclusion: The paper offers new ideas to approach the practical problems of automatic tuning, but some additional discussion addressing the issues mentioned above would increase its impact. It is probably more of a technology demonstration than purely scientific innovation. In my opinion, the paper will be of largest benefit for researchers designing new probes in the field of imaging and solid state NMR. It may also be a starting point for designing future high resolution / high sensitivity NMR probe systems.

Reviewer 2:

Authors: First of all, we would like to thank the reviewer very much for investing time and effort to review our manuscript.

Reviewer: General comments: The authors claim an automatic system for RF tuning and matching through a micro- controller (Arduino) and variable capacitors by mechanical step-motors. This reviewer acknowledges the need to develop automatic system to replace time-consuming manual adjustment. However, some points are not clear and mislead the readers so a minor revision is necessary to improve the quality of this manuscript to be published. Major and minor concerns are listed below.

Reviewer: Major concerns 1. This study is limited in receive coil only. As the authors state in part 2 (why tune and match?), the tuned and matched condition is matter even at receiving side. However, the effect of impedance matching at the transmit side is more important in SNR. There is no any comments about the transmit side, tuning and matching condition with sample.

Authors: In fact, the study is general and was applied to transceive (transmit/receive) coils. We are sorry if the relevant paragraph was not completely clear to convey that message. But in lines 50-55 we mention that the impedance of the coil and the spectrometer electronics (this implicitly includes transmitter and receiver) should match the characteristic impedance of the coaxial cables. Moreover, in that paragraph we stated that matching the coil to 50 Ohm maximizes the power transfer and thus guarantees efficient excitation field B₁. We definitely meant here the excitation phase of the NMR experiment. Furthermore, the experiments reported in this paper were all performed on transceive coils.

We have emphasized this point in the manuscript (lines: 56, 59, 60)

Reviewer: How can the authors verify the condition of the transmit is always same during all experiments for this work. Perhaps, dose it relate to #5 in minor con- cerns? Even very small difference at transmit side (distance between a sample and coil or between transmit and receive coil.) make a huge different results in S-parameters (S₁₁ and S₂₁) that ultimately make different SNR. The authors should explain how to keep the same condition to conduct the comparison of receive only coil among manual, before and after auto tune and match.

Authors: We think that this point was based on the assumption that we used different coils for Tx and Rx. If this were the case, then this concern would have been very valid and then careful attention must be paid to ensure that the transmitter conditions do not change. But as we mentioned in the first comment, in our experiments we used a single transceive coil. As such and as long as the sample does not change the transmit conditions will not change.

Reviewer: 2. Tuning and matching, in general, are performed after a sample is loaded. If the shift by loading a sample s negligible, this work has less scientific impact. Also, RF coils that have a little bit wide bandwidth may resolve the loading problems. In this respect, the authors are required supplement addition experiments to prove the necessity of this work. For example, bench test results with a universal tuning and matching before and after a sample loads to show

loading effect that should be compensated. Also, the authors can add an image and SNR comparison with a universal tuned and matched coil using a sample without manual and auto correction in figure 9.

Authors: As detailed in Hoult's paper (Hoult, D. I. (1979). Journal of Magnetic Resonance, 34, 425–433.) the sample-loading effect depends on many parameters including the coil geometry, coil parameters (R, L, C, Q), sample parameters, and the frequency of operation. To elaborate how large this effect can be, we did a couple of experiments and added two figures to the supplementary materials, which we also attach here as Fig 1 and Fig 2.

Figure 1: shows the unloaded/loaded S11 of a commercial 5 mm saddle coil designed to operate in a 11.7 T NMR magnet at 500 MHz. The sample we used was 0.5 M NaPO₃, 0.5 M Phosphoric Buffer Solution (PBS), 50 mM TSP, and 0.5 M Sucrose. Loading the sample showed a dramatic change (6 MHz frequency shift and 28 dB increase in the reflection) in the tuning and matching condition.

Figure 2: shows the NMR spectrum of the sample before and after readjusting the T&M condition. Readjusting the T&M condition showed a significant enhancement (6.4 times) of the SNR.

We have added a paragraph in the manuscript (lines: 20-22) and two figures in the supplementary (Fig1 and Fig2) to clarify this point.

Reviewer: 3. (Line 7, page2) and (Line 94, page 4): it misleads the readers because VCO may cover the frequency range for 1T to 23T but it is almost impossible to adjust resonating frequency (i.e., Larmor frequency) with capacitors and RF coil element. Otherwise, the authors should provide additional description with practical values (e.g., capacitor values and/or size of resonating structure) that can cover the wide range of NMR system.

Authors: Sorry for this confusion! What we wanted to say is that ArduiTaM can be used to automatically T&M almost every commercial probe. This is because it utilizes a programmable frequency synthesizer (ADF4351) capable of generating any frequency in the range from 35MHz to 4.4 GHz. So for example, ArduiTaM can T&M any of the following: a 300 MHz ¹H probe in a 7T magnet, a 125 MHz ¹³C probe in a 11.7T magnet, a 600 MHz ¹H probe in a 14.1T magnet, and so on. In all these examples, the T&M ranges are limited mainly by the trimmers of the probe (maximum tuning range is in the order of few MHz).

We have added a sentence (lines: 99-101) to clarify this point

Reviewer: Minor concerns 1. Is stepper motor okay for MRI study even if it has strong magnetic property? It may bring safety issues or magnetic field disturbance.

Authors: If the magnet is well shielded and if the motor is placed far enough then this shouldn't be a problem. In our experiment we used a 1T MRI permanent magnet and we placed the stepper motor outside the magnet where the average stray field is 500 uT. We didn't observe any forces or malfunction of the motor. Indeed, the Bruker sample changer system also uses similar stepper motors.

We have added a sentence (lines: 147, 148) to clarify this point

Reviewer: 2. (Line 24, page 2): Please add a reference in the bibliography about the commercial system.

Authors: Done.

Reviewer: 3. How can the NMR console receive a signal from ArduiTaM system? Is there an open port in the console or the homebuilt system need an interface module? The details should be described in the manuscript to better understanding because the minimized interface between automatic system and NMR console is important in this application.

Authors: From our experience of working with different NMR spectrometers, almost all systems provide a number of general purpose TTL inputs and outputs that can be easily programmed by the user to do various control and triggering tasks. For example, the Bruker preclinical MRI machine (ICON) has one TTL output trigger port and one TTL input trigger port. For imaging experiments using ParaVision, the TTL output trigger can be set in the pulse program using the commands "TTL1_HIGH" and "TTL1_LOW", while the TTL input can be used (by ticking a Checkbox in the GUI) to allow an external signal to trigger the signal acquisition.

We have added a sentence (lines: 47, 48) to address this point.

Reviewer: 4. There are some typo (e.g., line 28, page2) and improper English grammar/expression. The authors need to carefully check it.

Authors: Checking done.

Reviewer: 5. This reviewer would like to ask to the authors to add the mathematical analysis to explain SNR comparison in Line 158, page 13.

Authors: The formula we used to calculate the SNR loss due to ArduiTaM is $SNR_{loss} = \frac{SNR(\text{without ArduiTaM}) - SNR(\text{with ArduiTaM})}{SNR(\text{without ArduiTaM})} * 100$

Reviewer: How only 0.8 dB insertion loss results in lowering 6 dB in SNR in figure 9.

Authors: The SNR values mentioned in this figure are in linear scale. Thus, the loss in SNR is around 1.13 dB.

We have elucidated this in the manuscript (lines: 171, 172)

Reviewer: 6. Figure 5 missed the unit for the Y-axis.

Authors: We have changed this figure.

ArduiTaM: accurate and inexpensive NMR auto tune and match system

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Abstract. We introduce a low complexity, low cost, yet sufficiently accurate automatic tune and match system for NMR and MRI applications. The ArduiTaM builds upon an Arduino Uno embedded system that drives a commercial frequency synthesizer chip to perform a frequency sweep around the Larmor frequency. The generated low power signal is fed to the NMR coil, after which the reflected waves are detected using a directional coupler, and amplified. The signal shape is then
5 extracted by means of an envelope detector and passed on to the Arduino, which performs a dip search while continuously generating actuator control patterns to adjust the tune and match capacitors. The process stops once the signal dip reaches the Larmor frequency. The ArduiTaM works readily with any spectrometer frequency in the range from 1 T to 23 T. The speed of ArduiTaM is mainly limited by the clock of the Arduino, and the capacitor actuation mechanism. The Arduino can easily be replaced by a higher speed micro controller, and varactors can replace stepper-motor controlled variable capacitors. The
10 ArduiTaM is made available in open source, so is easily duplicated.

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1 Introduction

Nuclear magnetic resonance spectrometers for imaging and spectroscopy are predominantly operated with inductor-capacitor (LC) resonators that pick up the radio frequency signal due to the evolving spin magnetisation in a sample or patient. Because
15 the detected NMR signals are naturally very weak, it is of utmost importance that high quality-factor components are used along the analogue radio frequency signal path, so as to minimise signal losses.

Proper tuning and matching (T&M) of the NMR probe is also important, and when done properly as will be demonstrated in the following section, this significantly enhances the receiver's sensitivity, thereby reducing the signal averaging times that would otherwise be required to obtain sufficient signal-to-noise ratio.

20 [As detailed in Hoult \(1979\), sample loading can significantly alter the electrical properties of the NMR coil and thereby disturb its tuning-and-matching condition \(see figure 1 in the supplementary\). Therefore, the NMR coil is usually re-tuned and](#)

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re-matched after loading a new sample. In many NMR/MRI systems, T&M is done manually by mechanically adjusting two trimmer capacitors. Although this hands-on process has been acceptable for many years, the need for automatic procedures has become important with the trend towards high-throughput experiments, for example so that samples can be automatically loaded into the magnet and analysed without delay.

The major commercial system providers recently started offering add-ons to equip their probes with automatic tuning and matching. These systems contain actuation units that drive the mechanical trimmer capacitors of the probe and are, in turn, controlled by the spectrometer software, which uses a so-called wobble routine to obtain the feedback signal. The offered solutions are costly and therefore only practical for probes with a limited number of channels. A further drawback is that the commercial systems are designed to drive mechanical trimmers, and therefore not adaptable to tuning and matching customised probes that for example involve digital capacitors or varactors. Moreover, these commercial systems are further limited by the capabilities of the RF channels of the spectrometer, and thus lack the generality needed by the experimentalist. So for instance, an automatic T&M system installed in an NMR spectrometer with a ^1H narrow-band channel cannot be used to T&M a ^{13}C coil, or *vice versa*.

To overcome these limitations, we considered the availability of off-the-shelf analogue and digital electronic components needed for such a system. In this paper, we report our findings, and present a compact low-cost accurate Arduino-based automatic tuning and matching system, abbreviated as ArduiTAM. Unlike commercial solutions and previously published reports Hwang (1998); Koczor (2015); Muftuler (2002); PerezdeAlejo (2004); Sohn (2015, 2013) that use either the MR spectrometer or a commercial network analyser for frequency generation and signal processing, our system employs a single chip frequency source covering a useful range of 35 MHz to 4.4 GHz, as well as discrete signal processing electronics, rendering it a completely standalone system capable of tuning and matching almost any relevant NMR/MRI probe channel. The ArduiTAM is compatible with most NMR spectrometers, can readily be interfaced via two TTL lines (almost all NMR/MRI systems provide general purpose TTL inputs and outputs that can be arbitrarily programmed by the user), and requires neither software add-ons (like Koczor's work Koczor (2015)) nor hardware alterations. The spectrometer-probe can thus be brought back to its original state by simply detaching the unit.

The ArduiTAM accomplishes T&M using the same principle that one would apply manually, namely, it monitors the signal reflected from the probe (S_{11}), then varies the tune and match capacitors until the minimum signal reflection amplitude occurs at the Larmor frequency. This gives it the advantage of being completely independent of the probe's topology, thereby eliminating constraints on the probe, such as the orthogonality of tuning and matching considered in Hwang's paper Hwang (1998). Furthermore, the ArduiTAM can, apart from NMR/MRI experiments, be a handy tool in any RF laboratory, useful to characterise coils, coil arrays, antennas, and impedance matching networks.

2 Why tune and match?

In almost all commercial NMR systems the spectrometer electronics racks are placed adjacent to the magnet due to their relatively large dimensions. This necessitates the use of shielded coaxial cables to guide the NMR signals from the coil to the

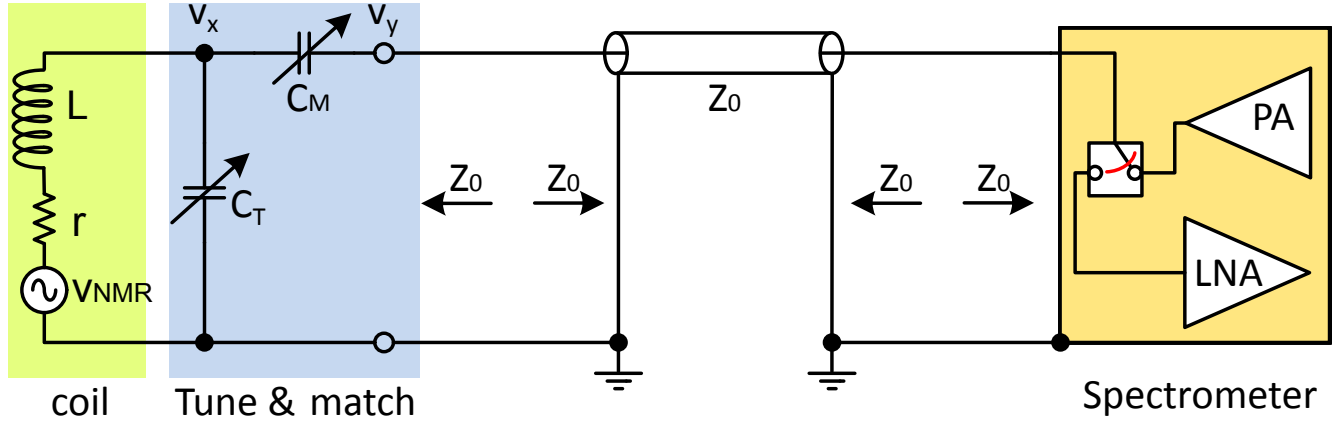


Figure 1. Example of a widely used parallel-tune/series-match topology. The L-matching circuit converts the complex impedance of the coil to a purely resistive impedance equal to the characteristic impedance of the coaxial cable, Z_0 .

55 spectrometer. The coaxial cables usually have a characteristic impedance, Z_0 , of $50\ \Omega$, and therefore all RF components of the NMR spectrometer (such as the power amplifier of the transmitter and the low-noise amplifier of the receiver) are designed accordingly to ensure impedance matching and consequently maximise power transfer. The NMR coil is no exception, and the use of a $50\ \Omega$ coaxial cable to connect the coil to the spectrometer implicitly implies that it also must be matched to Z_0 to guarantee an efficient excitation field, B_1 , in the excitation phase, and an efficient signal acquisition in the reception phase of the NMR experiment. The impedance matching of the NMR coil also minimises the signal reflection coefficient Γ

$$\Gamma = \frac{Z_{\text{coil}} - Z_0}{Z_{\text{coil}} + Z_0}, \quad (1)$$

and thus prevents the formation of standing waves in the cables Mispelter (2006).

Matching the coil impedance is commonly realised using high quality, almost lossless, capacitors, as illustrated in figure 1. As such, the matching process also implies that the coil will be part of a resonant circuit, hence the term "tuning". The process of tuning and matching the coil in figure 1 can be performed as follows: first, C_T is varied to make the coil resonate at a frequency, ω_r , slightly above the Larmor frequency, ω_l , such that the real impedance of the parallel resonator is $50\ \Omega$ at ω_l . Then, the residual imaginary impedance, which in this case is inductive, can be eliminated by varying C_M . In effect, the extra capacitance is the complex conjugate of the residual inductance. This process results in the coaxial cable experiencing a purely resistive $50\ \Omega$ load impedance at ω_l . Due to resonance, the tuning and matching network acts, in what can be considered as one of its major advantages, as a passive noiseless preamplifier, thus $|v_y| = G_{\text{TM}} \cdot |v_{\text{NMR}}|$, with the tune and match voltage gain $G_{\text{TM}} = 0.5\sqrt{Z_0/r}$. According to Friis' formula,

$$F_{\text{Total}} = 1 + \frac{F_{\text{receiver}} - 1}{G_{\text{TM}}}, \quad (2)$$

this particular feature can significantly lower the noise factor F (noise figure $\text{NF} = 10\log F$) of the NMR receiver and thus enhance its sensitivity (see figure 2 in the supplementary).

75 To obtain an impression of how significant this can be, consider the circuit in figure 2a as an example of a typical MR receive channel. The circuit uses the LMH6629 low noise amplifier from Texas Instruments® in a non-inverting topology. The operation frequency of the circuit is arbitrarily set to 500 MHz and the T&M capacitors are assumed to be noiseless. The circuit was simulated using the Advanced Design System software (ADS) to explore the effect that T&M the NMR coil will have on the overall signal-to-noise ratio. Figure 2b shows the voltage amplification, $G_{\text{TM}} = |v_y/v_{\text{NMR}}|$, due to T&M, while figure 2c demonstrates the ratio of the output SNR with T&M, to that without T&M, for different values of the coil's AC resistance. The latter figure clearly shows how T&M can significantly enhance the SNR. The enhancement falls off as the coil's noise increases. For a coil with a relatively high AC resistance of, say $5\ \Omega$, T&M still results in an SNR enhancement by a factor of more than 2. Thus improper T&M results not only in an inefficient power transfer during transmission, but also in an increase in the NF during reception, leading to a severe loss of sensitivity.

85 3 ArduiTaM implementation

The ArduiTaM requires hardware and software co-design, which is detailed in this section.

3.1 Circuit design

Figure 3 depicts the block diagram of the ArduiTaM circuit, for the case of T&M capacitors that are rotated using stepper motors. This figure also describes how the ArduiTaM is easily inserted in the signal path of a spectrometer, underlining its integrability. It requires minimal connections, namely, a TTL trigger signal from the spectrometer to the Arduino, and a TTL acknowledgement signal from the Arduino back to the spectrometer, to facilitate automation. After loading a new sample, the spectrometer can thus trigger the ArduiTaM to readjust the T&M of the probe. Once the ArduiTaM is done, it will send an acknowledgement signal back to the spectrometer so as to start the NMR experiment. The ArduiTaM circuit consists of an Arduino Uno as the master controller, carrying out the frequency sweep control, signal acquisition, signal processing, optimum T&M condition search, and the adjustment of the variable capacitors. The Arduino furthermore allows the user to set the channel Larmor frequency, as well as the frequency sweep range for tuning and matching. The ArduiTaM uses an ADF4351 high-quality ultra-wideband frequency synthesizer from Analog Devices® to generate the required frequency sweeps. The synthesizer is controlled using an SPI protocol, and covers a frequency range from 35 MHz to 4.4 GHz, making ArduiTaM compatible with the frequencies of almost any commercial NMR spectrometer available today. So for example, ArduiTaM can T&M any of the following: a 300 MHz ^1H probe in a 7 T magnet, a 125 MHz ^{13}C probe in a 11.7 T magnet, a 600 MHz ^1H probe in a 14.1 T magnet, and so on.

The output of the synthesizer is transferred to the NMR probe through a low-loss directional coupler (ZFDC-10-1 from Mini-Circuits®), and then through a high quality (low insertion loss and high isolation) RF switch (ZFSWA-2-46 from Mini-Circuits®). The latter is used to toggle between the "T&M mode" in which the NMR probe is connected to the ArduiTaM, and the "NMR mode" in which the probe is connected to the NMR spectrometer, and is the only additional lossy element that is active during NMR signal acquisition (also refer to Figure 9).

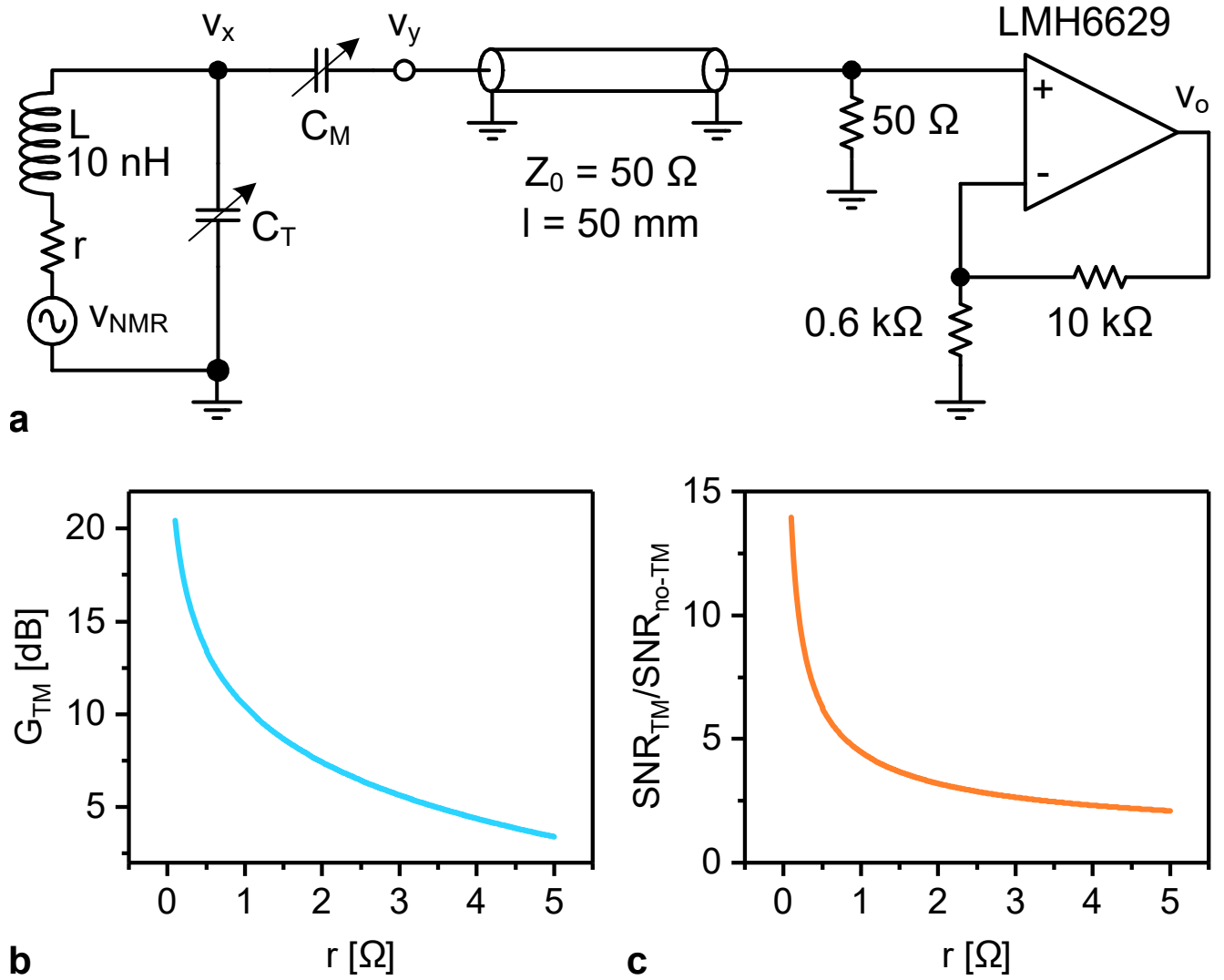


Figure 2. The effect of T&M the NMR coil on the overall signal-to-noise ratio after the receiver. (a) Typical NMR receiver circuit including the coil, T&M capacitors, coaxial cable, and low-noise amplifier. The cable length was set to be short enough so that its attenuation is negligible. (b) The passive amplification, G_{TM} , as a function of the coil's resistance. (c) The overall SNR enhancement as a function of the coil's resistance. All simulations were performed using the Advanced Design System (ADS) software.

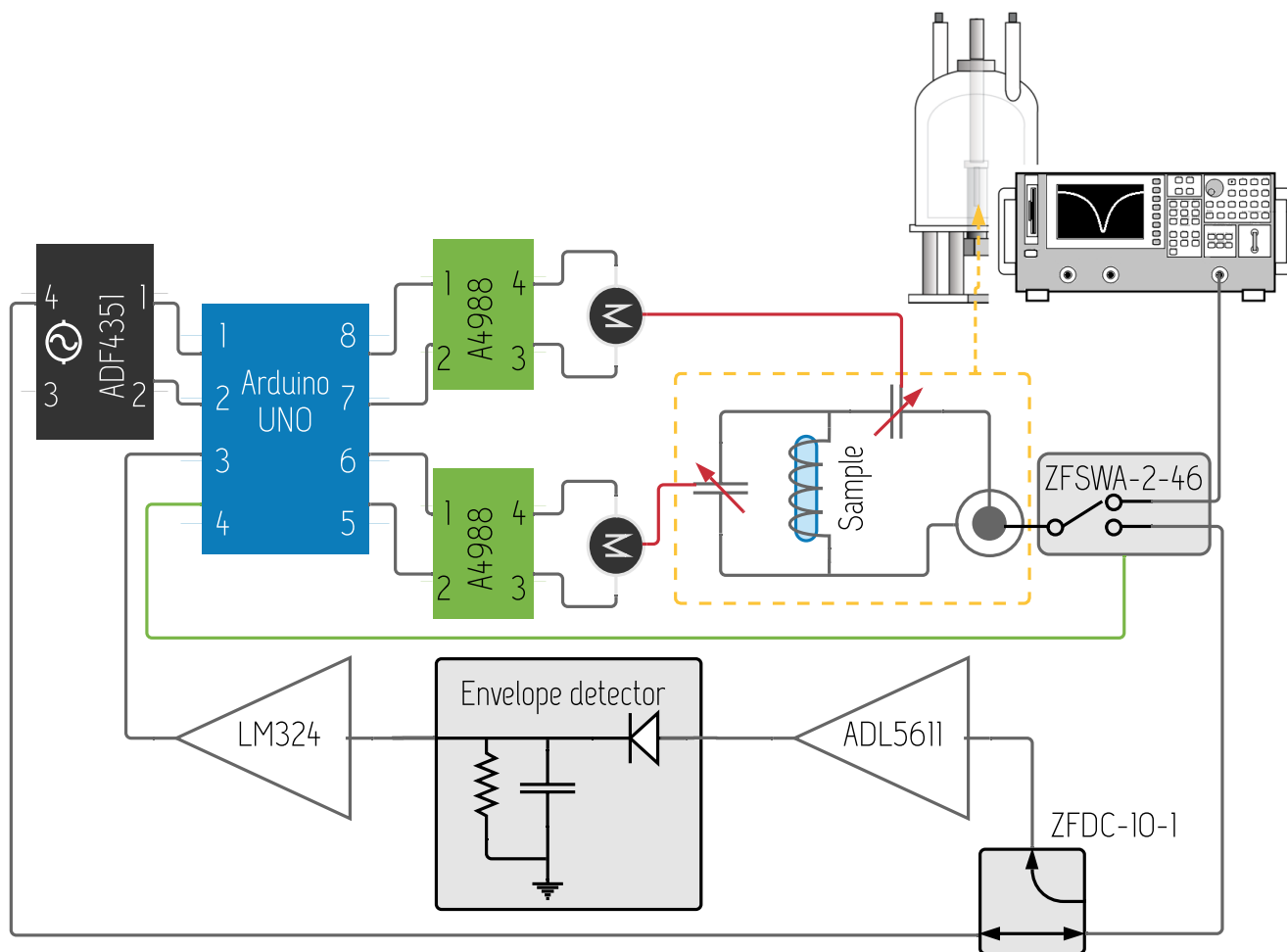


Figure 3. Block diagram of the ArduiTAM, detailing its component interconnections, as well as how the system can be inserted in the signal path of a spectrometer.

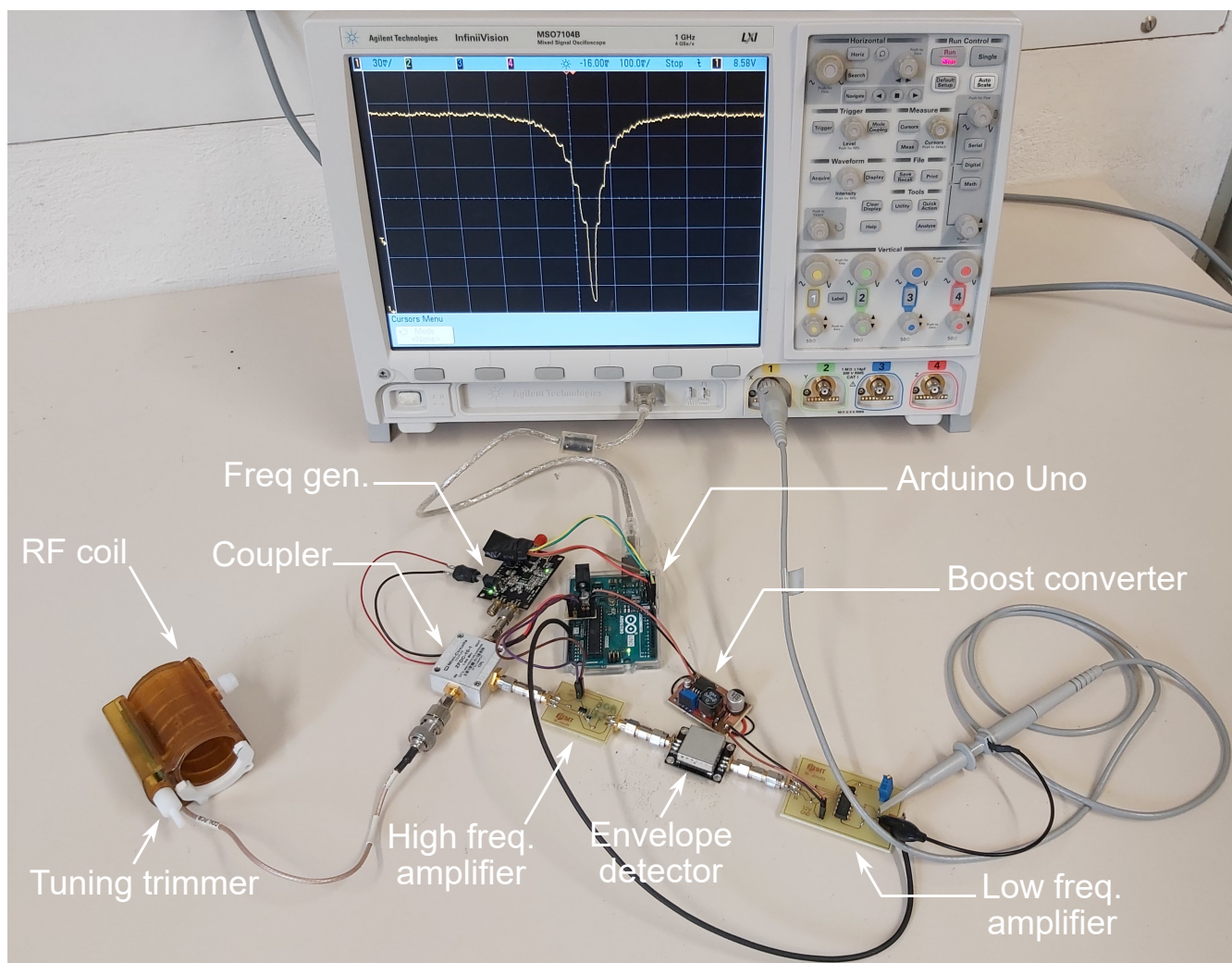


Figure 4. The experimental setup of the ArduiTAM showing the acquired S_{11} signal of the coil on the oscilloscope.

The reflected signal from the probe is taken from the coupler and amplified using an ADL5611 from Analog Devices® (all circuit schematics are available in the supplementary files). After that, the envelope of the reflected signal is extracted using a high sensitivity (-40 dBm) pin-diode-based envelope detector. The extracted envelope represents the probe's signal reflection, or S_{11} -curve, and is further amplified using an LM324 with an explicit low-pass filter of 200 Hz bandwidth to eliminate high frequency residuals. The low frequency S_{11} -curve is acquired by the Arduino through one of its analogue inputs, and the auto T&M algorithm is executed based on the acquired data. Figure 4 shows the interconnected discrete components of the ArduiTaM in which an oscilloscope was used to visualise the acquired S_{11} curve of the coil, verifying performance. Figure 5 displays four acquisitions of the S_{11} curves recorded by the Arduino for two cases; when the tuning capacitor, C_T , of the coil is (a) fixed, and (b) arbitrarily changed. The results demonstrate the robustness and reliability of the circuit.

3.2 Tuning algorithm

Before and after the T&M protocol runs, a trigger signal is sent to and from the Arduino microcontroller to toggle between two modes of operation: T&M, and NMR measurement by the host system. Once the start trigger signal is received, the algorithm initialises all variables and resets the position of the capacitors, C_t and C_m , to their minimum value using a so-called "homing routine". The routine causes the stepper motors to turn counterclockwise until they reach a lower angle limit, corresponding to the lowest value of the trimmer capacitors. Afterwards, the user is asked to enter the desired Larmor frequency, f_0 , for which the tuning and matching conditions will be sought.

The algorithm sweeps the tuning capacitances against fixed values for the matching capacitances, capturing the S_{11} values for each combination. S_{11} values are read from an analogue input of the microcontroller at which the already amplified and extracted envelope signal is input. To reduce the algorithm's running time, the first sweep is done at a low resolution, with a sweep step size of $S_{sw} = 64 \cdot S_m$, where S_m represents a single step of the stepper motor, which is equivalent to the inverse of the steps per turn, referred here as spt , that a stepper motor can provide. Our prototype uses motors with $spt = 200$, resulting in $S_m = 1.8^\circ$. Once the first sweep is complete, the capacitor pair $\{C_t, C_m\}$ with the lowest S_{11} value (S_{11min}) is found and a new searching window is defined. The chosen search intervals are symmetric around S_{11min} with a span of S_{sw} in each direction i.e., $S_{11min} \pm S_{sw}$, for which the corresponding tuning and matching capacitor values are already known. The same cycle is run four consecutive times, increasing the resolution by 4 with respect to the previous cycle until the maximum resolution of rotational increment is reached, that is, $S_{sw} = S_{sw}/4$ until $S_{sw} = S_m$ (see Fig. 6). Ultimately, the algorithm's resolution is limited by S_m , which can be easily improved with the use of stepper motors with a higher spt value, or through the use of a step down gear box. After the last cycle, the motors are positioned at the angles for which tuning and matching capacitances corresponded to the lowest probe reflection. Finally, the microcontroller activates the RF switch and sends a trigger signal to the NMR spectrometer to switch to NMR measurement mode. The current implementation requires the user to do one-time single-point calibration of the tuning and matching capacitors when attaching ArduiTaM for the first time. This can be easily done by manually rotating the trimmers to their lower values which are recognised by ArduiTaM as the zero positions, and by setting the allowed number of turns before upper values are reached. As long as it is not turned off, ArduiTaM can keep track of stepper motors' positions and ensure that neither limit is exceeded. A simple modification of the code, such that current positions the trimmers are written

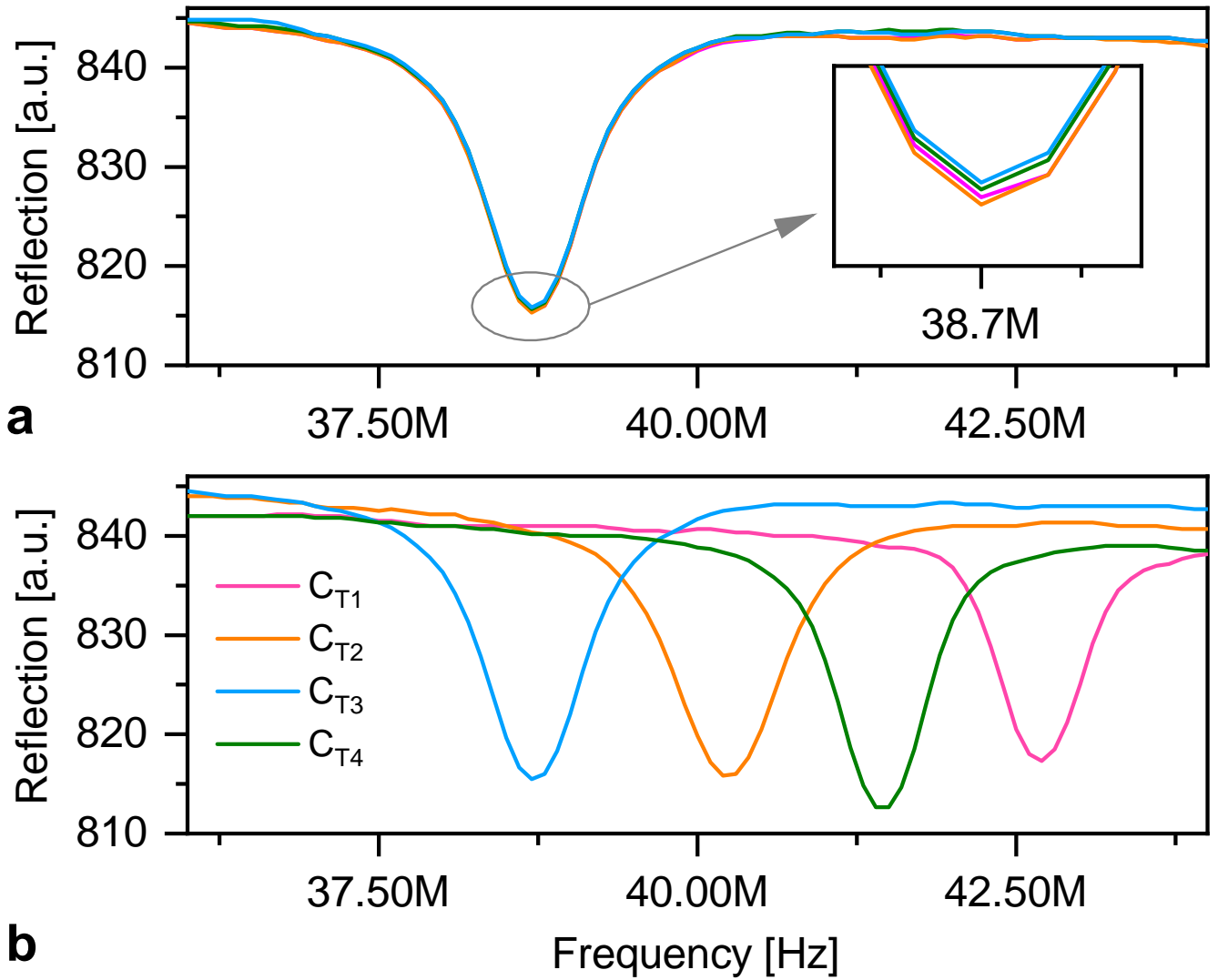


Figure 5. (a) Four consecutive acquisitions of S_{11} , by ArduiTaM, of a coil with fixed C_T value. The overlaid curves were acquired via one of the analogue inputs of the Arduino. The x-axis covers the frequency range of the sweep. The y-axis represents the magnitude of the reflected signal. The insert zooms in onto the minimum of the curves. (b) S_{11} of the same coil with four arbitrarily different C_T values.

in the EEPROM of the Arduino, would allow ArduiTaM to keep track of the motors' positions even after being completely powered off.

4 Results

The ArduiTaM was first tested on a homemade RF coil. The solenoid was designed to operate in a 1.055 T preclinical MRI magnet at a Larmor frequency of 44.93 MHz. We used two sapphire dielectric trimmers, each with 28-turn threads (56π rad), covering a range of 0.5 pF to 10 pF, to tune and match the coil according to the circuit topology depicted in figure 2. Two stepper motors were used to mechanically drive the trimmers, see figure 7a. In order to avoid potential mutual interactions, the motors were placed outside the magnet where the average stray field is around 500 μ T. In this setup we explored two scenarios:

1. The two trimmers were arbitrarily set, and ArduiTaM was applied. Covering a tuning and matching range of 6 turns for each trimmer, and using 4 loops of resolution (corresponding to a final step of approximately 32 fF), ArduiTaM could precisely T&M the coil in 2 min and 24 s. Figure 7b shows the S_{11} -curve of the coil before and after applying ArduiTaM.
2. The matching capacitor of the coil was adjusted to achieve an optimum matching at the Larmor frequency, whereas the tuning capacitor was arbitrarily set. Covering a wider sweep range of 9 turns with a finer resolution through 6 loops, ArduiTaM was capable of precisely tuning the coil, figure 7c, in 22 s.

The speed of rotation of the stepper motors was kept conservatively low to protect the capacitors from mechanical damage, which affected the time of the measurement. The S_{11} measurements in figure 7 were obtained using a Keysight E5071C network analyser. In order to highlight its practicality, we applied ArduiTaM to a commercial probe (Bruker ICON) as shown in figure 8a. The probe is designed such that its matching condition is always met over the entire range of targeted samples. Therefore, it exhibits a tuning capacitor only. We used an RF switch (ZFSWA-2-46), controlled by the TTL output of the MRI scanner, to toggle between the T&M mode where ArduiTaM runs, and the MRI mode in which the scanner's electronics are routed to the coil. Figure 8b plots the percentage of reflection from the coil, recorded using the standard "wobble" routine of the scanner, for three cases; first, when the coil was manually tuned, second, when the coil was arbitrarily de-tuned, and third, when the coil was automatically re-tuned using ArduiTaM. The tuning range, the number of resolution loops, and thus the tuning time (22 s) were similar to the values used in figure 7c. In order to assess the effect of ArduiTaM on the performance of a commercial system, we conducted an imaging experiment of a cherry tomato with and without applying ArduiTaM, see figure 9. For both experiments, we utilised a standard gradient-echo sequence with a 1 mm slice thickness, 312 μ m in-plane resolution, 30° flip angle (FA), 4 ms echo time (TE), 100 ms repetition time (TR), and averaging 8 times. Moreover, to ensure that both experiments have exactly the same initial settings, we ran the automatic adjustment routines before each experiment. These include a "drift adjustment" to correct the frequency drift caused by the field drift, a "power adjustment" to calculate the correct power that corresponds to the desired flip angle, and a "receiver gain adjustment" to calculate the receiver gain that ensures optimum digitisation of the signals. The measured linear-scale SNR before applying ArduiTaM, figure 9(left) is 49,

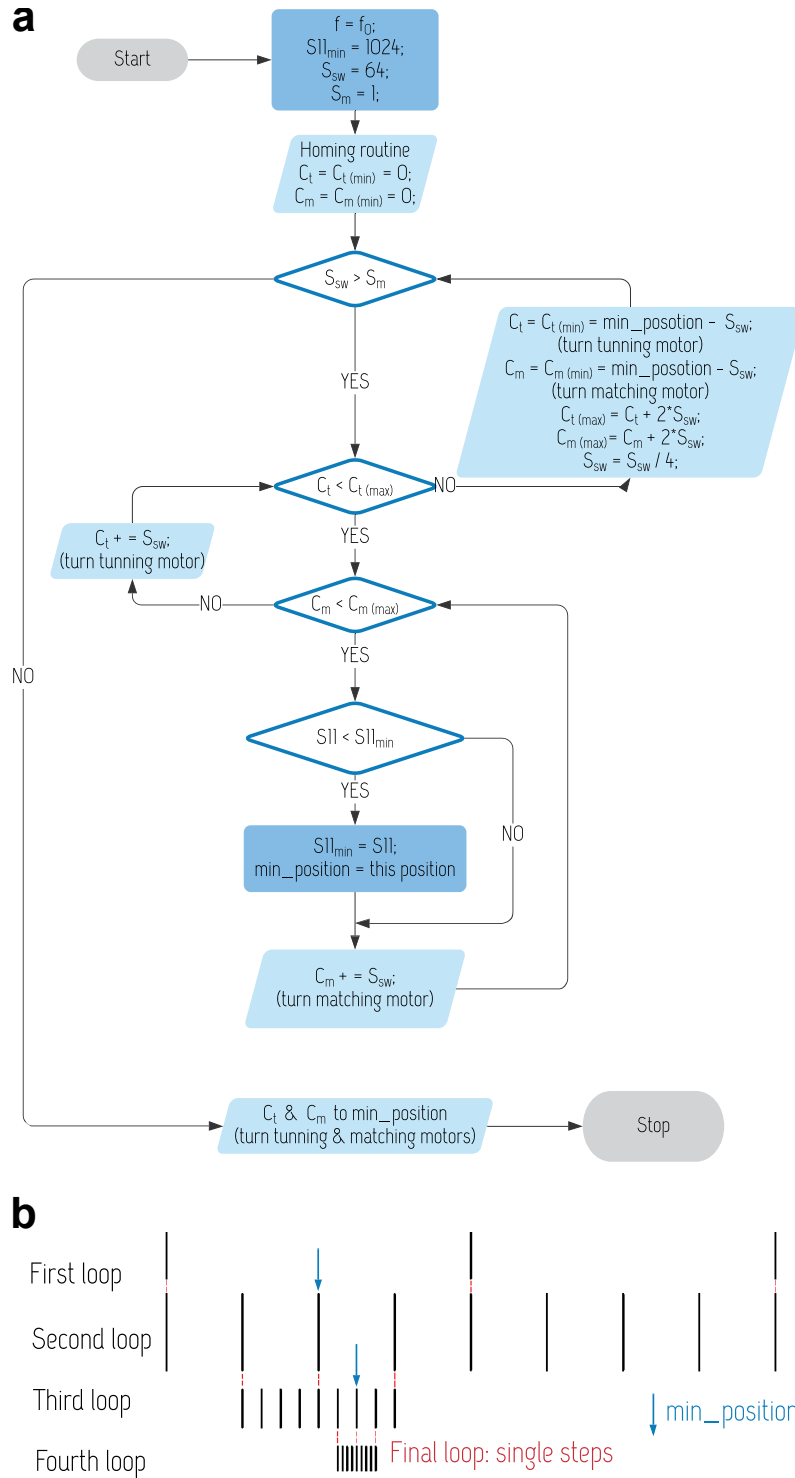


Figure 6. (a) T&M flowchart. (b) Schematic showing the interval subdivision method to zoom in on the S_{aa} minimum.

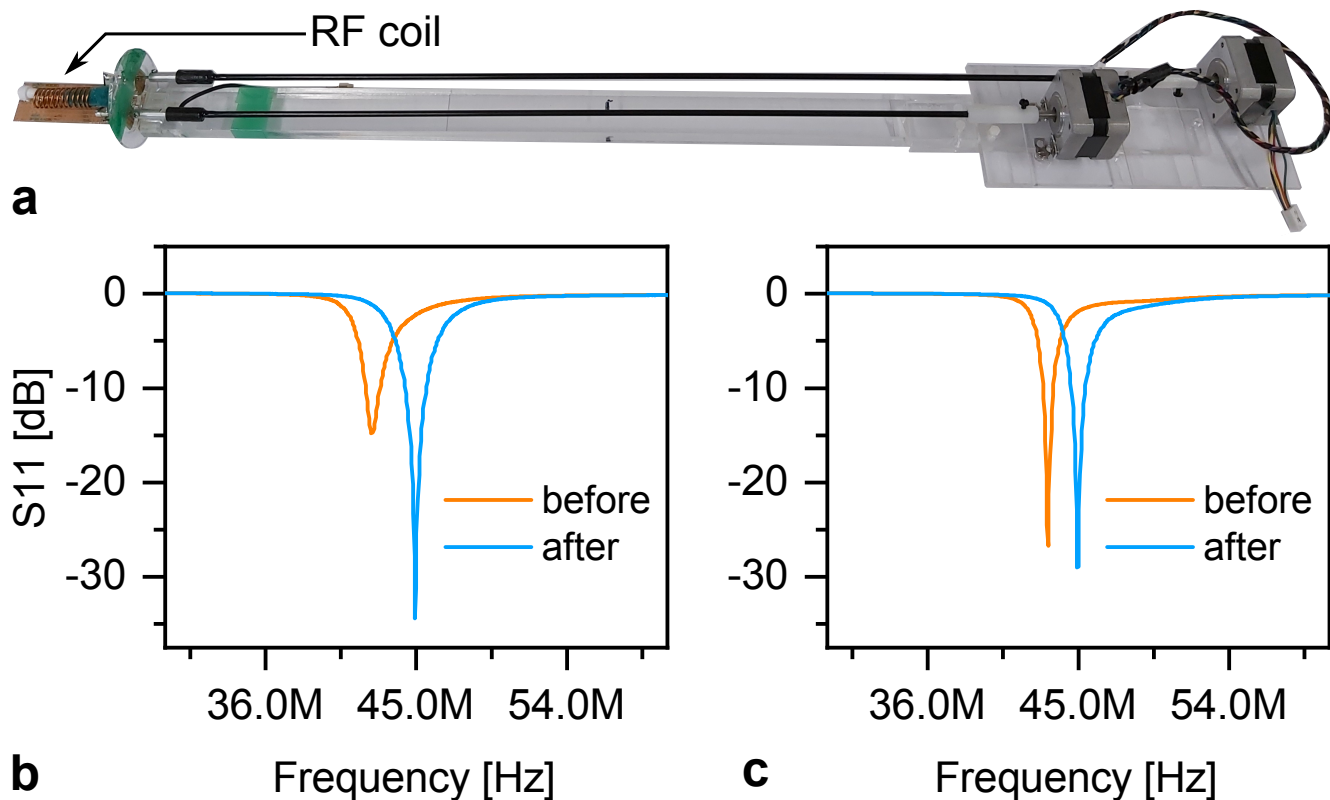


Figure 7. (a) Homemade RF coil with a mechanical setup for automatic T&M. The coil operates at a Larmor frequency of 44.93 MHz. (b) Result of applying ArduiTaM to T&M the coil starting from an arbitrary condition. (c) Result of applying ArduiTaM to adjust the tuning capacitor only.

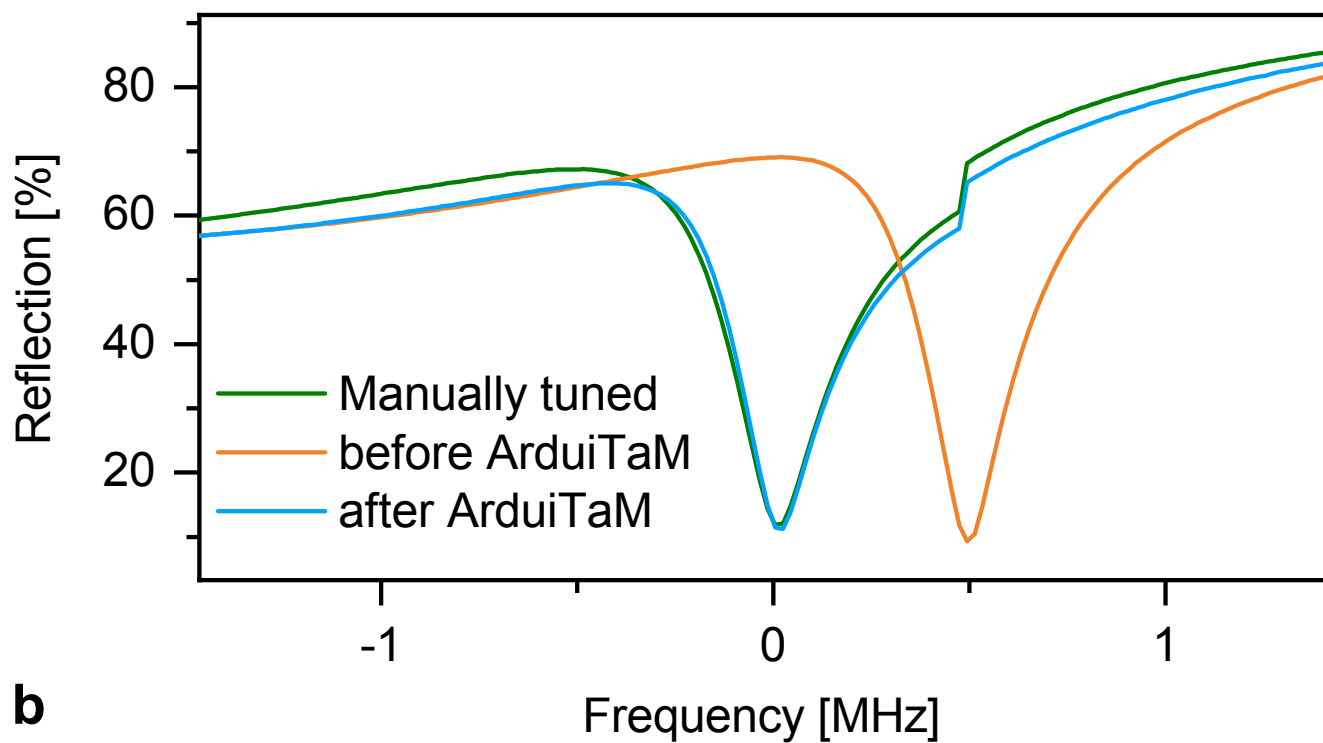
while the SNR after inserting ArduiTaM, figure 9(right), is 43 corresponding to a 12 % (1.13 dB) loss in the signal-to-noise ratio. The slight loss in SNR is due to the insertion loss of the RF switch (0.8 dB) needed by ArduiTaM to route the RF signals.

5 Conclusions

ArduiTaM is a fully functional automatic tuning and matching system for use in NMR or MRI systems. Despite its simplicity, ArduiTaM exhibits high precision, reliability, and most importantly, a negligible influence on NMR signal fidelity. By utilising an ADF4351 frequency synthesizer, ArduiTaM is completely independent of the spectrometer, and conveniently covers a frequency range of 35 MHz to 4.4 GHz, making it compatible with most commercial NMR or MRI frequencies. Moreover, its very low cost (around 100 Euros for the chip components at the time of writing) makes it particularly attractive for use with multi-resonant probes and MRI phased arrays. Away from MR, other potential applications, such as antennas, resonators, and impedance matching networks, may stand to benefit as well.



a



b

Figure 8. (a) Integrating ArduiTaM with a commercial MRI probe (Bruker ICON). (b) "Wobble" curves showing the coil's reflection when it is manually tuned, and before and after the automatic tuning using ArduiTaM.

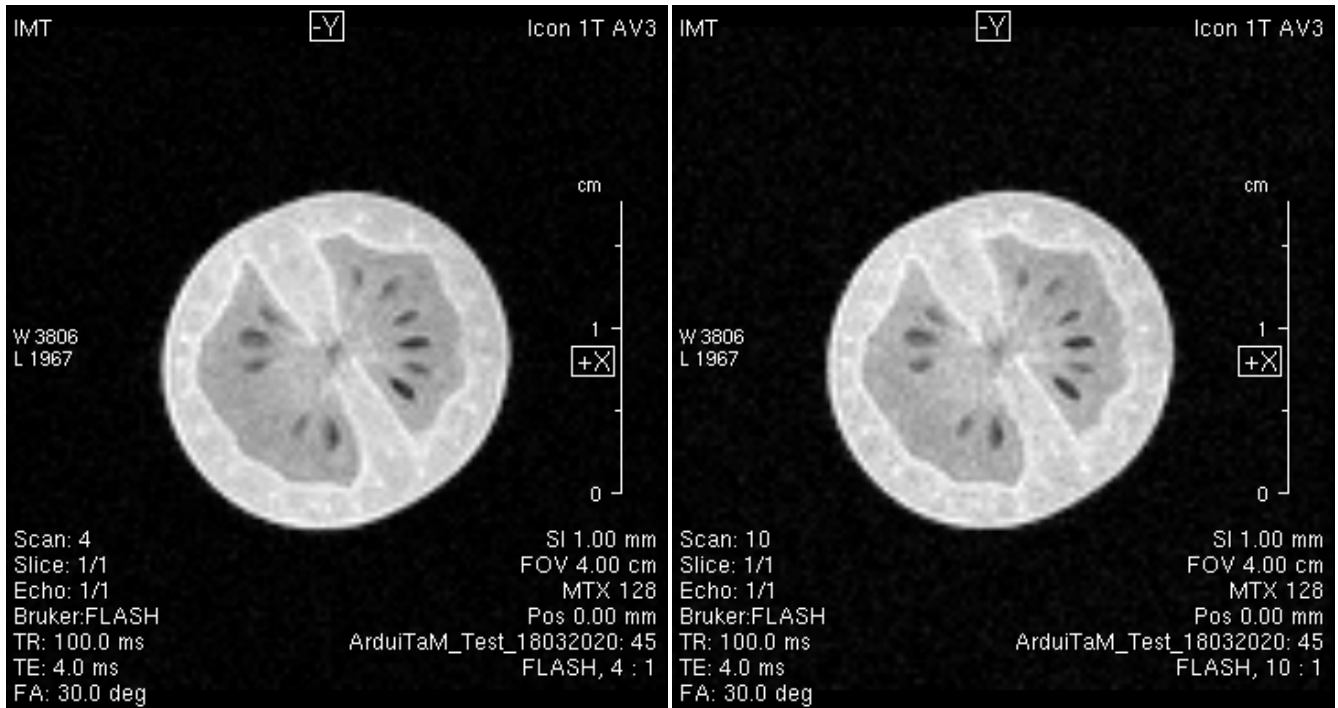


Figure 9. Integrating ArduiTaM with a commercial MRI scanner shows only a negligible effect on its performance. (Left) MR image of a cherry tomato before applying ArduiTaM. The measured SNR is 49. (Right) Repeating the same experiment after applying ArduiTaM. The measured SNR here is 43, reflecting a loss of approximately 12 %, due to the insertion loss of the RF switch (ZFSWA-2-46 from Mini-Circuits®).

ArduiTaM was successfully tested on a homemade coil prototype that uses stepper-motor-driven trimmer capacitors for tuning and matching. Trimmers were purposely employed to demonstrate ArduiTaM’s ease of integrability with commercial systems, where such capacitors are predominantly used. Unfortunately, the use of mechanical trimmers imposes a limit on the speed of T&M. However, trimmers can easily be replaced with varactors or digitally-tuned capacitors (DTCs), for much faster tuning and matching. The speed of T&M can be further optimised depending on the experiment. So, for example, if the maximum frequency shift happens to be known for the samples under test, then the sweep ranges can be minimised so that ArduiTaM can make more rapid adjustments.

Code and data availability. All circuit schematics are provided in the supplementary file. The Arduino codes are available under: <https://github.com/mazinjouda/ArduiTaM.git/>.

Author contributions. Concept initialisation: MJ and JGK. Circuit design, implementation, and test: MJ. Tune and match algorithm: SMTD and DM. Writing the Arduino codes: SMTD. Building and testing the mechanical setups: MAJ. Final measurements: MJ. Funding request and supervision: JGK. Writing, review, and editing: MJ, SMTD, MAJ, DM, and JGK.

Competing interests. The authors declare no competing interests.

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References

- Hwang, F., Hoult, D.I.. Automatic probe tuning and matching. *Magn Reson Med* 39, 214–222, <http://doi.org/10.1002/mrm.1910390208>, 1998.
- 200 Koczor, B., Sedyó, I., Rohonczy, J.. An alternative solution for computer controlled tuning and matching of existing NMR probes. *J Magn Reson* 259, 179–185, <https://doi.org/10.1016/j.jmr.2015.08.017>, 2015.
- Mispelter, J., Lupu, M., Briguet, A.. *NMR probeheads for bio-physical and biomedical experiments: theoretical principles & practical guidelines*. Imperial College Press, 2006.
- Muftuler, L.T., Gulsen, G., Sezen, K.D., Nalcioğlu, O. Automatic tuned MRI RF coil for multinuclear imaging of small animals at 3T. *J Magn Reson (San Diego, Calif. : 1997)* 155, 39–44, <https://doi.org/10.1006/jmre.2002.2510>, 2002.
- 205 Pérez de Alejo, R., Garrido, C., Villa, P., Rodriguez, I., Vaquero, J.J., Ruiz-Cabello, J., Cortijo, M.. Automatic tuning and matching of a small multifrequency saddle coil at 4.7 T. *Magn Reson Med* 51, 869–873, <http://doi.org/10.1002/mrm.20045>, 2004.
- Sohn, S.M., DelaBarre, L., Gopinath, A., Vaughan, J.T.. Design of an Electrically Automated RF Transceiver Head Coil in MRI. *T Biomed Circ S.*, <http://doi.org/10.1109/TBCAS.2014.2360383>, 2015.
- 210 Sohn, S.M., DelaBarre, L., Vaughan, J.T., Gopinath, A. 8-Channel RF head coil of MRI with automatic tuning and matching, in: 2013 IEEE MTT-S. pp. 1–3, <http://doi.org/10.1109/MWSYM.2013.6697681>, 2013.
- Hoult, D. I., Lauterbur, P. C.. The Sensitivity of the Zeugmatographic Experiment. *J. Magn. Reson.* 34, 425–433, [https://doi.org/10.1016/0022-2364\(79\)90019-2](https://doi.org/10.1016/0022-2364(79)90019-2), 1979.